Ceram. Soc. 9 (1967) 131.

- 5. N. DOUKHAN, R. DUCLOS and B. ESCAIG, J. *Phys.* C 9 (1973) 379.
- 6. P. VEYSSIÈRE, J. RABIER, H. GAREM and J. GRILHE, Phil. Mag., to be published.

Received 1 July and accepted 28 August 1975

The effect of silica on the nitridation o f silicon

The sensitivity of the reaction between high purity silicon and nitrogen to the nature of the surrounding alumina reaction tubing has been reported $[1]$. Observations based on the use of four types of alumina suggested that contaminants released from the alumina at nitridation temperature influenced the course of the reaction to favour formation of the beta-phase of silicon nitride. Nitridations have now been carried out using commercial grades of silicon powder in similar reaction environments. These confirm that the alumina must be regarded as a reaction variable (Fig. 1), but also suggest that the action of these contaminants may be more complex than had previously been assumed.

The characteristics of the silicon powders are given in Table I. Nitrogen gas was purified using an acidified aqueous chromous chloride scrubber, and phosphorus pentoxide. Small (approximately

Figure I Reaction extent after 6 h for silicon powder D, plotted against temperature, using two grades of alumina reaction tube.

9 19 76 Chapman and Hall Ltd. Printed in Great Britain.

J. RABIER P. VEYSSIERE J. GRILHÉ

Laboratoire de Métallurgie Physique, $Faculté$ des Sciences. *40, Avenue du Recteur Pineau, 86022 Poittiers, France*

10 mm diameter \times 10 mm length) compacts of silicon powder were nitrided inside short inner tubes of two types of commercial sintered alumina (designated A and B), the ends of which were packed with discs of zirconium foil. The reaction system was evacuated to 10^{-6} bar at temperature and then nitrogen Filled before the inner tube and specimens were drawn magnetically into the hot zone. Pellet green densities were approximately 1600 kg m^{-3} , and the nitrogen flow rate was 10 ml $min⁻¹$. The extent of nitridation was determined by measurement of initial and final weights, and the proportion of alpha- and beta-phases in the product by means of Philips diffractometer.

Results from nitridations in tubes of alumina B for which reaction time was varied at constant temperature (1365° C) are shown in Fig. 2. It is apparent that almost all the alpha-phase forms in the initial stage of the reaction, and that the bulk of the beta-phase is formed later, in conjunction with the characteristic slight upturn in the reactiontime curve. That prolonged nitridation may lead to a decreased alpha/beta ratio of the products is a common observation [2, 3], but the possibility of dividing the nitridation process into two fairly clearly defined stages has apparently not been commented on.

If the oxygen is assumed to be present initially as a uniform silica film on the silicon grains a

thickness of the order of 2 nm would be required. At 1365° C the reactions

$$
SiO2(s) + Si(s) \approx 2SiO(g)
$$

$$
SiO2(s) \approx SiO(g) + \frac{1}{2}O2(g)
$$

provide equilibrium partial pressures of silicon monoxide and oxygen of approximately 4×10^{-3} and 10^{-20} bar respectively. Evaporation of silica would be expected to occur provided the oxygen pressure were maintained below approximately 2×10^{-3} bar and the silicon monoxide were continuously removed. These values will of course be only a guide to the actual pressures because of the essentially non-equilibirum nature of the system, and the small percentage of other oxides and silicates present.

It would appear, therefore, that the formation of the alpha-phase of silicon nitride can be associated with the existence of silica (or silicon monoxide) within the nitriding compact. When loss of surface silica by evaporation is complete the reaction may accelerate, but due almost entirely to an increased rate of production of the beta-phase. It has been suggested that solid state diffusion processes are relatively insignificant in the silicon nitridation reaction, and that the dominant mechanism is that of the vapour phase transport of reactants, with interaction taking place at suitable nuclei, or nitride surfaces [4]. These results imply that when silicon is carried to the reaction site as silicon monoxide the alpha-phase develops; when the silicon is present as silicon vapour, only the beta-phase is produced.

BO , r , **I00'** Powder D (Alumina B) bO $*_{\infty}$ 80 40 **6o** reaction extent $/2$ -20 40 + Wp ò -~ **20** W_{α} Z C , i i i , i i i i i i , i i i **I6** 0 2 4 6 8 I0 12 14 SiO₂ additions wt%

Figure 3 The effect of silica additions to silicon powder D on reaction extent and product yield, after 6 h at 1365[°] C.

Supporting evidence for a relationship between the presence of silicon monoxide and the formation of the alpha-phase is contained in the results of experiments in which small percentages of silica (B.D.H. precipitated grade) were incorporated in the silicon powder compacts, also nitrided in tubes of alumina B. The beta-forming reacting is markedly retarded although the alpha-forming reaction is relatively unaffected (Fig. 3). This effect is also seen in the reference compacts of silicon (without silica addition), placed alongside the mixed samples in the zirconium gettered reaction tube (Fig. 4). The probable explanation for the action of this added silica is that in providing background partial pressures of silicon monoxide and oxygen, it suppresses the evaporation of silica from the silicon surfaces, and prolongs the slower "alpha-stage" of the reaction. It is well-known that the alpha-phase can be prepared by the large scale reaction between silicon monoxide and nitrogen [5], and the involvement of silicon monoxide in powder nitridations has long been suspected [6].

This work indicates that the presence of oxygen aids the formation of the alpha-phase. Earlier results, however, have shown that the phase can be formed in gettered high purity systems in which only traces of oxygen were likely to have been present [7], and crystals have now been prepared having oxygen contents close to zero [8]. Taken together these facts suggest that the main function of the oxygen is that of a silicon carrier, and that it is the form in which the silicon arrives at a developing nitride surface which determines the crystal structure. This is additional evidence that the alpha and beta phases of silicon nitride should

Figure 4 Reaction extent and product yield after 6 h for reference compacts of powder D , nitrided at 1365 $^{\circ}$ C together with silica-containing compacts (Fig. 3).

be regarded as polymorphs, the beta phase having the slightly lower energy [9]. The concentration, and type, of impurity in the nitriding system, or the form in which silicon is supplied to the growing nucleus, appear to control which phase develops although only very small amounts of these other components may be incorporated in the crystal structure. In this respect silicon nitride would be showing features broadly similar to those of silicon carbide, for which vapour phase impurities have been found to favour strongly growth of hexagonal structures as opposed to that of the cubic structure [10]. Many other examples of this phenomenon are of course known [11].

Alternative mechanisms for the action of metallic impurities in affecting the proportions of alpha- and beta-nitride formed, besides the possible direct assistance of the beta-phase formation, now have to be considered. One possibility is that the oxides operate in part by accelerating the volatilization and ultimate disappearance of silica films. Another is that by combining with silica, silicon monoxide partial pressures are reduced relative to that of silicon vapour. It is clear that the overall course of the nitridation of a specific silicon powder is likely to be determined in a complex way by both oxygen and metallic impurity levels, and that these two factors are unlikely to operate independently.

Acknowledgements

The assistance of H. P. Rooksby in the interpretation of X-ray diffraction data is gratefully acknowledged, as are the support grants from UNESCO, and the Spanish Association of Mining Engineers, to D. Campos-Loriz.

References

- 1. R. B. GUTHRIE and F. L. RILEY, *J. Mater. Sci. 9* (1974) 1363.
- 2. W. NARUSE, M. NOJIRI and M. TADA, *Nihon Kinzoku gakkaishi* 35 (1971) 731.
- 3. P. LONGLAND, University of Leeds, private communication.
- 4. A. ATKINSON, A. J. MOULSON and E. W. ROBERTS, *J. Mater. Sci.* 10 (1975) 1242.
- 5. K. KIJIMA, N. SETAKA, M. ISHII and H. TANAKA, *J. Amer. Ceram. Soc.* 56 (1973) 346.
- 6. N. L. PARR and E. R. W. MAY, *Proc. Brit. Ceram. Soc.* 7 (1967) 81.
- 7. R. B. GUTHRIE and F. L. RILEY, *ibid* 22 (1973)

275.

- 8. K. KIJIMA, K. KATO, Z. INOUE and H. TANAKA, *J. Mater. Sci.* 10 (1975) 362.
- 9. C. M. B. HENDERSON and D. TAYLOR, *Trans. J. Brit. Ceram. Soc.* 74 (1975) 49.
- I0. W. F. KNIPPENBERG and G. VERSPUI, *Mat. Res. Bull.* 4 (1969) 533.
- 11. H. E. BUCKLEY, "Crystal Growth" (Chapman and Hall, London, 1951) p. 383.

Received 9 July and accepted 29 July 1975

> D. CAMPOS-LORIZ F. L. RILEY *Department of Ceramics, Houldsworth School of Applied Science, University of Leeds, Leeds, UK*

Metals, Ceramics and Polymers

An Introduction to the Structure and Properties of Engineering Materials

OLIVER H. WYATT and DAVID DEW-HUGHES

An undergraduate textbook in which the authors have combined their understanding of the physical and engineering aspect of the subject in a unique book containing many novel approaches.

'... **one of the very best of the many Englishlanguage texts on materials that have appeared in recent years.'** *Nature*

'... **can be recommended for all types of engineers involved with materials which means the greater part of the profession'** *The Chemical Engineer*

Hard covers £15.00 net Paperback £6.90 net

Fracture of Brittle Solids

B. R. LAWN and T. R. Wl LSHAW

The aim of this book is to provide an integrated view of brittle fracture theory, building on the fundamental energy-balance concepts originally laid down by Griffith. Emphasis is placed on basic principles rather than factual detail, with the behaviour of 'model' materials providing illustrative examples. The treatment is suitable for senior undergraduate and graduate students and research workers in materials science and related disciplines.

Cambridge Solid State Science Series **Hard covers £7.20 net Paperback £3.80 net**

CAMBRIDGE UNIVERSITY PRESS